**Building Name: Dolby Regeneration** 

Medicine

**CAAN ID: 3047** 

Auxiliary Building ID: IRM Building



FORM 1

CERTIFICATE OF SEISMIC PERFORMANCE LEVEL

IN UC-Designed & Constructed Facility

☐ Campus-Acquired or Leased Facility

#### **BUILDING DATA**

Building Name: Dolby Regeneration Medicine (includes structurally independent pedestrian bridge connecting to HSIR tower)

Address: 35 Medical Center Way

Site location coordinates: Latitude 37.7618 Longitudinal -122.4581

#### UCOP SEISMIC PERFORMANCE LEVEL (OR "RATING"): |||

ASCE 41-17 Model Building Type:

a. Longitudinal Direction: S2: Ordinary Concentrically Braced Frames with Base Isolation

b. Transverse Direction: S2: Ordinary Concentrically Braced Frames with Base Isolation

Additional: Bridge contains independent trussed steel tower and steel piers cantilevered from the foundation

Gross Square Footage: 68,765 Number of stories *above* grade: 0

Number of basement stories below grade: 3

Year Original Building was Constructed: 2010
Original Building Design Code & Year: CBC-2007

Retrofit Building Design Code & Code (if applicable): NA

#### SITE INFORMATION

Site Class: C Basis: (Forell/Elesser, 9/30/2010, S0.0.1)

Geologic Hazards:

Fault Rupture: No
Liquefaction: No
Basis: UCSF Presumptive Buildings – Geotechnical Assessment, Egan (2019)
Basis: UCSF Presumptive Buildings – Geotechnical Assessment, Egan (2019)
Basis: UCSF Presumptive Buildings – Geotechnical Assessment, Egan (2019)

#### **ATTACHMENT**

Original Structural Drawings: (Institute of Regeneration Medicine Building, Forell/Elesser, 9/30/2010,

S0.0.1) or

Seismic Evaluation: NA

Retrofit Structural Drawings: NA

Date: 8/16/2019

Building Name: Dolby Regeneration

Medicine

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#### **CERTIFICATION & PRESUMPTIVE RATING VERIFICATION STATEMENT**

I, Maryann T. Phipps, a California-licensed structural engineer, am responsible for the completion of this certificate, and I have no ownership interest in the property identified above. My scope of review to support the completion of this certificate included both of the following ("No" responses must include an explanation):

a) the review of structural drawings indicating that they are as-built or record drawings, or that they

an explanation):
<ul> <li>a) the review of structural drawings indicating that they are as-built or record drawings, or that the otherwise are the basis for the construction of the building: ✓ Yes □ No</li> <li>b) visiting the building to verify the observable existing conditions are reasonably consistent with those shown on the structural drawings: ✓ Yes □ No</li> </ul>
Based on my review, I have verified that the UCOP Seismic Performance Level (SPL) is presumptively permitted by the following UC Seismic Program Guidebook provision (choose one of the following):
☑ 1) Contract documents indicate that the original design and construction of the aforementioned building is in accordance with the benchmark design code year (or later) building code seismic design provisions for UBC or IBC listed in Table 1 below.
$\Box$ 2) The existing SPL rating is based on an acceptable basis of seismic evaluation completed in 2006 or later.
$\square$ 3) Contract documents indicate that a comprehensive building seismic retrofit design was fully-constructed with an engineered design based on the 1997 UBC/1998 <i>or later</i> CBC, and (choose one of the following):
□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1E (or BSE-R) and BSE-2E (or BSE-C) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 CBC <i>or later</i> for EXISTING buildings, and is presumptively assigned an SPL rating of IV.
□ the retrofit project was completed by the UC campus. Further, the design was based on ground motion parameters, at a minimum, corresponding to BSE-1 (or BSE-1N) and BSE-2 (or BSE-2N) as defined in ASCE 41, or the full design basis ground motion required in the 1997 UBC/1998 <i>or later</i> CBC for NEW buildings, and is presumptively assigned an SPL rating of III.
$\Box$ the retrofit project was not completed by the UC campus following UC policies, and is presumptively assigned an SPL rating of IV.

Date: 8/16/2019

<sup>&</sup>lt;sup>1</sup> A comprehensive retrofit addresses the entire building structural system as indicated by the associated seismic evaluation, as opposed to addressing selective portions of the structural system.

Building Name: Dolby Regeneration

Medicine

**CAAN ID: 3047** 

Auxiliary Building ID: IRM Building



Date: 8/16/2019

#### **CERTIFICATION SIGNATURE**

Maryann T. Phipps
Print Name
Title

S2995
CA Professional Registration No.
License Expiration Date

Maryann J. Hipps
Signature

AFFIX SEAL HERE

PROFESSION
PROFESSION
No. 2995
EXP. 6/30/20

Signature

AFFIX SEAL HERE

PROFESSION
PROFESSION
No. 2995
EXP. 6/30/20

Signature

Date

Estructure, (510) 235-3116, 1144 65th St Suite A, Oakland

Firm Name, Phone Number, and Address

**Building Name: Dolby Regeneration** 

Medicine

**CAAN ID: 3047** 

Auxiliary Building ID: IRM Building



Date: 8/16/2019

Table 1: Benchmark Building Codes and Standards

Building Type a,b	Building Seismic Design Provisions	
	UBC	IBC
Wood frame, wood shear panels (Types W1 and W2)	1976	2000
Wood frame, wood shear panels (Type W1a)	1976	2000
Steel moment-resisting frame (Types S1 and S1a)	1997	2000
Steel concentrically braced frame (Types S2 and S2a)	1997	2000
Steel eccentrically braced frame (Types S2 and S2a)	1988 <sup>g</sup>	2000
Buckling-restrained braced frame (Types S2 and S2a)	f	2006
Metal building frames (Type S3)	f	2000
Steel frame with concrete shear walls (Type S4)	1994	2000
Steel frame with URM infill (Types S5 and S5a)	f	2000
Steel plate shear wall (Type S6)	f	2006
Cold-formed steel light-frame construction—shear wall system (Type CFS1)	1997 <sup>h</sup>	2000
Cold-formed steel light-frame construction—strap-braced wall system (Type CFS2)	f	2003
Reinforced concrete moment-resisting frame (Type C1) <sup>i</sup>	1994	2000
Reinforced concrete shear walls (Types C2 and C2a)	1994	2000
Concrete frame with URM infill (Types C3 and C3a)	f	f
Tilt-up concrete (Types PC1 and PC1a)	1997	2000
Precast concrete frame (Types PC2 and PC2a)	f	2000
Reinforced masonry (Type RM1)	1997	2000
Reinforced masonry (Type RM2)	1994	2000
Unreinforced masonry (Type URM)	f	f
Unreinforced masonry (Type URMa)	f	f
Seismic isolation or passive dissipation	1991	2000

Note: This table has been adapted from ASCE 41-17 Table 3-2. Benchmark Building Codes and Standards for Life Safety Structural Performed at BSE-1E.

Note: UBC = Uniform Building Code. IBC = International Building Code.

<sup>&</sup>lt;sup>a</sup> Building type refers to one of the common building types defined in Table 3-1 of ASCE 41-17.

<sup>&</sup>lt;sup>b</sup> Buildings on hillside sites shall not be considered Benchmark Buildings.

c not used

<sup>&</sup>lt;sup>d</sup> not used

e not used

 $<sup>^{\</sup>it f}$  No benchmark year; buildings shall be evaluated in accordance with Section III.J.

<sup>&</sup>lt;sup>g</sup> Steel eccentrically braced frames with links adjacent to columns shall comply with the 1994 UBC Emergency Provisions, published September/October 1994, or subsequent requirements.

<sup>&</sup>lt;sup>h</sup> Cold-formed steel shear walls with wood structural panels only.

 $<sup>^{\</sup>it i}$  Flat slab concrete moment frames shall not be considered Benchmark Buildings.

- CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE CALIFORNIA BUILDING CODE, 2007 EDITION.
- DETAILS OF THE CONSTRUCTION NOT FULLY SHOWN OR NOTED ON THE DRAWINGS NOR CALLED FOR IN THE SPECIFICATIONS SHALL BE OF THE SAME SIZE AND CHARACTER AS FOR SIMILAR CONDITIONS WHICH ARE SHOWN AND NOTED.
- 4. THE WORD "TYPICAL" SHALL MEAN THAT THE INDICATED INFORMATION SHALL BE APPLIED TO ALL SIMILAR CONDITIONS WHETHER OR NOT THE INFORMATION IS SPECIFICALLY REFERENCED, UNLESS NOTED OTHERWISE ON THE DRAWINGS
- THE CONTRACTOR SHALL VERIFY ALL EXISTING CONDITIONS AND DIMENSIONS AT JOB SITE. THE CONTRACTOR SHALL COMPARE STRUCTURAL DRAWINGS WITH ARCHITECTURAL, CIVIL, LANDSCAPE, MECHANICAL, PLUMBING, AND ELECTRICAL DRAWINGS BEFORE COMMENCING WITH THE WORK AND SHALL NOTIFY THE ARCHITECT OF ANY DISCREPANCIES REQUIRING CLARIFICATION OR REVISION. DO NOT SCALE DRAWINGS.
- 5. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR THE SAFETY AND PRESERVATION OF THE BUILDING AND CONTENTS DURING CONSTRUCTION, AND SHALL BE SOLELY RESPONSIBLE FOR PROVIDING A SAFE PLACE TO WORK. THE CONTRACTOR SHALL EXECUTE WORK TO ENSURE SAFETY OF PERSONS AND PROPERTY AGAINST DAMAGE BY FALLING DEBRIS AND OTHER HAZARDS IN CONNECTION WITH THIS WORK, AND SHALL PROVIDE ADEQUATE SHORING AND BRACING DURING ALL DEMOLITION AND CONSTRUCTION.

### **DESIGN BASIS**

THE DESIGN IS IN ACCORDANCE WITH THE CALIFORNIA BUILDING CODE, 2007 EDITION AND PROVIDES FOR THE FOLLOWING LOADS:

40 PSF

35 PSF

45 PSF

10 PSF

50 PSF

100 PSF

100 PSF

### DEAD LOADS

SLAB AND FRAMING WEIGHTS AS SHOWN ON THE PLANS

### SUPERIMPOSED DEAD LOADS

OFFICE & MECHANICAL

LABORATORY (GREEN) 80 PSF **FLOORS LABORATORIES** 30 PSF

MECHANCIAL STAIRS & RAMPS

OFFICES

LIVE LOADS

OFFICE & MECHANICAL LABORATORY (GREEN) 50 PSF BRIDGE 20 PSF LABORATORIES 80 PSF CORRIDORS, STAIRS, RAMPS 100 PSF MECHANICAL 50 PSF

WIND LOADS

OFFICE

BRIDGE

LOADING DOCK

BASIC WIND SPEED = 85 MPH EXPOSURE CATAGORY = C qh = 20 psf

 $GCpi = \pm 0.18$ 

h = 60 ft

SEISMIC LOADS V (NORTH-SOUTH) = 0.14 W 0.14 W V (EAST-WEST) = Cs (NORTH-SOUTH) = 0.06 g Cs (EAST-WEST) =  $0.06\,\mathrm{g}$ SEISMIC DESIGN CATAGORY = OCCUPANCY CATAGORY =

Sms = 1.285 gSm1 = 0.85 gSOIL TYPE = So Sds = 0.855 gSd1 = 0.565 g

SEISMIC LOAD RESISTING SYSTEMS

NORTH -SOUTH DIRECTION: STEEL ORDINARY CONCENTRICALLY BRACED FRAME (OCBF)  $R = 1.0 \Omega_0 = 1.0$ 

EAST-WEST DIRECTION:

STEEL ORDINARY CONCENTRICALLY BRACED FRAME (OCBF) R = 1.0  $\Omega_0$  = 1.0 THE SEISMIC LOAD RESISTING SYSTEMS CONSIST OF THE STEEL BRACED FRAME BEAMS AND COLUMNS, COLLECTORS, METAL DECK ROOFS AND FLOORS AND OTHER DRAWING SHEETS AND DETAILS NOTED AS SLRS. COLLECTORS ARE THOSE BEAMS NOTED ON THE PLANS TO HAVE

DOUBLE ROW OF BOLTING OR SPECIAL COLLECTOR CONNECTIONS AT ONE OR BOTH ENDS.

## **NON-STRUCTURAL COMPONENTS**

 $Fp = U_{ave} \frac{Sp}{R_p/I_p} W$ 

 $a_p = SEE ASCE 7-05$ 

 $u_{ave} = 0.3g AT LEVELS 9 & 10$ = 0.6g AT OFFICE ROOFS

 $R_0 = SEE ASCE 7-05$ (USE Ip = 1.5 FOR COMPONENTS REQUIRED FOR LIFE SAFETY OR

## DRILLED CONCRETE PILES

REFER TO GEOTECHNICAL REPORT, AS LISTED IN THE FOUNDATIONS SECTION OF THE GENERAL NOTES, FOR DRILLED PILE CRITERIA AND RECOMMENDATIONS.

CONTAINING HAZARDOUS MATERIALS)

2. ALLOWABLE VERTICAL CAPACITIES FOR DRILLED PILES ARE AS FOLLOWS:

DEAD LOAD + LIVE LOAD 10.0 KSF DEAD PLUS LIVE + SEISMIC (OR WIND) LOAD 13.3 KSF UPLIFT LOAD 8.9 KSF

- 3. SEE GEOTECHNICAL REPORT FOR DRILLED PILE LATERAL SHEAR AND BENDING DESIGN CURVES.
- 4. DRILLED PILES SHALL BE INSPECTED AND APPROVED BY THE UNIVERSITY'S GEOTECHNICAL ENGINEER PRIOR TO CONCRETE PLACEMENT.

### SPECIAL INSPECTION

THE SPECIAL INSPECTION REQUIREMENTS OF CHAPTER 17 OF THE CALIFORNIA BUILDING CODE, 2007 EDITION, APPLY TO THE FOLLOWING:

- STEEL CONSTRUCTION
- CONCRETE CONSTRUCTION
- ANCHORS AND DOWELS IN RESIN
- EXPANSION ANCHORS
- SOILS PILE FOUNDATIONS
- THE SUPPLEMENTAL SPECIAL INSPECTION REQUIREMENTS FOR SEISMIC RESISTANCE OF CBC SECTION 1707 APPLY TO THE FOLLOWING ELEMENTS OF THE SEISMIC LOAD RESISTING SYSTEM
- STRUCTURAL STEEL
- PILE FOUNDATIONS

AND ARCHITECTURAL COMPONENTS:

ARCHITECTURAL COMPONENTS:

EXTERIOR NON-BEARING COLD-FORMED STEEL WALLS

THE SUPPLEMENTAL STRUCTURAL TESTING REQUIREMENTS FOR SEISMIC RESISTANCE OF CBC SECTION 1708 APPLY TO THE FOLLOWING ELEMENTS OF THE SEISMIC LOAD RESISTING SYSTEM:

 STRUCTURAL STEEL SEISMICALLY ISOLATED STRUCTURES

### STRUCTURAL OBSERVATION

STRUCTURAL OBSERVATION FOR SEISMIC RESISTANCE SHALL BE PROVIDED IN ACCORDANCE WITH CBC SECTIONS 1702 AND 1709. AT THE CONCLUSION OF THE STRUCTURAL WORK, THE OBSERVER SHALL SUBMIT A WRITTEN STATEMENT TO THE BUILDING OFFICIAL THAT THE SITE VISITS HAVE BEEN MADE AND IDENTIFY ANY REPORTED DEFICIENCIES THAT. TO THE BEST OF THE STRUCTURAL OBSERVER'S KNOWLEDGE, HAVE NOT BEEN RESOLVED.

### GEOTECHNICAL INFORMATION

- 1. THE UNIVERSITY'S GEOTECHNICAL ENGINEER, RUTHERFORD & CHEKENE, HAS PREPARED AN INVESTIGATION REPORT FOR USE ON THIS PROJECT, TITLED: "UPDATED DRAFT REPORT, GEOTECHNICAL INVESTIGATION, INSTITUTE FOR REGENERATIVE MEDICINE, UNIVERSITY OF CALIFORNIA, SAN FRANCISCO, CALIFORNIA", DATED 22 JANUARY 2008. LATERAL LOAD ANALYSES FOR DRILLED CONCRETE PILES WERE ALSO PROVIDED ON JULY 17, 2008 AND AUGUST 20, 2008.
- 2. THE CONTRACTOR SHALL REVIEW AND UNDERSTAND THE INFORMATION CONTAINED IN THE REPORT, BUT SHALL NOT ASSUME THAT SUCH INFORMATION IS SUFFICIENT FOR THE CONTRACTOR'S PURPOSES.
- 3. THE CONTRACTOR SHALL BE FAMILIAR WITH THE GEOTECHNICAL CONDITIONS AT THE
- 4. THE CONTRACTOR SHALL BE RESPONSIBLE TO OBTAIN GEOTECHNICAL REPORT AND INFORMATION NECESSARY TO COMPLETE THE WORK.
- 5. THE CONTRACTOR SHALL OBTAIN THE SERVICES OF AN INDEPENDENT GEOTECHNICAL ENGINEER LICENSED IN THE STATE OF CALIFORNIA TO ANALYZE AVAILABLE INFORMATION AND TO MAKE ADDITIONAL INVESTIGATIONS AS NECESSARY TO COMPLETE THE WORK.

### **FOUNDATIONS**

- REFER TO GENERAL NOTES SECTION TITLED "GEOTECHNICAL INFORMATION"
- 2. SLABS ON GRADE AND FOUNDATIONS SHALL BEAR ON APPROVED NATIVE SUBGRADE OR COMPACTED SOIL.
- PILE CAPS, FOOTINGS AND GRADE BEAMS SHALL BE CAST IN NEAT TRENCHED EXCAVATIONS (1" MINIMUM WIDER THAN SCHEDULED). IF FOOTINGS CANNOT BE CAST IN TRENCHES, FORM FOOTINGS TO SCHEDULED DIMENSIONS.
- DRAWINGS AND MAY BE REVISED BY THE UNIVERSITY'S GEOTECHNICAL ENGINEER TO ENSURE MINIMUM FOOTING EMBEDMENTS OF TWO FEET INTO FIRM, APPROVED SOIL MATERIAL (UNDISTURBED NATURAL SOILS OR COMPACTED ENGINEERED FILL). TOP OF FOOTING DIMENSION FROM DATUM SHALL BE AS SHOWN ON PLANS.

BOTTOM OF FOOTINGS SHALL BE CALCULATED USING INFORMATION SHOWN ON THE

- COMPACTED NATURAL SOIL, FILL, AND BACKFILL IS TO BE UNIFORMLY COMPACTED WITH APPROVED COMPACTION EQUIPMENT. FILL MATERIAL AND OPERATIONS SHALL BE INSPECTED BY THE OWNER'S GEOTECHNICAL ENGINEER.
- 6. WATER SHALL NOT BE ALLOWED TO STAND IN TRENCHES OR FORMS BEFORE OR AFTER CONCRETE IS PLACED, AND SHALL BE PUMPED OUT. IF BOTTOMS OF TRENCHES BECOME SOFTENED DUE TO RAIN OR OTHER WATER BEFORE FOOTINGS ARE CAST, THE CONTRACTOR SHALL EXCAVATE THE SOFTENED MATERIAL AND REPLACE WITH CONCRETE.
- 7. ALLOWABLE BEARING PRESSURES FOR SPREAD FOOTINGS:

DEAD PLUS LIVE LOAD = 3000 PSF

TOTAL LOAD (INCLUDING SEISMIC) = 4000 PSF

8. CANTILEVER RETAINING WALL DESIGN PRESSURE: 40 PCF

9. BASEMENT WALLS (RESTRAINED AT THE TOP) DESIGN PRESSURE: 60 PCF

10. SEISMIC SOIL INCREMENT: 15H PSF

- 11. DO NOT BACKFILL BASEMENT WALLS UNTIL ATTACHED CONSTRUCTION IS COMPLETE AND CONCRETE SLAB AND FILL ON METAL DECK OF SUPPORTING LEVELS HAS ATTAINED ITS 28-DAY STRENGTH.
- 12. SPECIAL INSPECTION REQUIREMENTS APPLY TO FILL AND BACKFILL OPERATIONS. FOOTING EXCAVATIONS SHALL BE INSPECTED AND APPROVED BY THE UNIVERSITY'S GEOTECHNICAL ENGINEER PRIOR TO PLACING REINFORCEMENT STEEL.

## POST-TENSIONED THREADBARS

POST-TENSIONED THREADBARS SHALL BE ASTM A-722 GRADE 150 HIGH TENSILE ALLOY STEEL. ACCESSORIES PROVIDED BY MANUFACTURER SHALL INCLUDE MACHINED ANCHOR PLATES, DOME-HEAD ANCHOR NUTS, FLEXIBLE GALVANIZED METAL SHEATHS, COUPLERS AND GROUT TUBES. THREADBARS SHALL BE POST-TENSIONED TO CONFORM TO THE FOLLOWING TENSILE STRESS LEVELS:

AT JACKING: 120 KSI (MAX) 105 KSI (MAX) AT TRANSFER: LONG-TERM (AFTER ALL LOSSES) 90 KSI (MIN)

SPECIFICATIONS.

THREADBARS SHALL BE FULLY GROUTED WITH APPROVED CEMENT GROUT FOLLOWING INSPECTION OF STRESSING AND APPROVAL OF STRESSING RECORDS. STRESSING END ANCHORS SHALL BE COATED WITH APPROVED RUST-PREVENTIVE PAINT, AND BLOCKOUTS SHALL BE FILLED SOLIDLY WITH APPROVED PEA-GRAVEL CONCRETE, IN ACCORDANCE WITH THE

### STRUCTURAL STEEL

WELDED HEADED STUDS

1. STEEL MATERIALS SHALL CONFORM TO THE FOLLOWING:

ASTM A 992 W-SHAPES, WT-SHAPES ASTM A 36 CHANNEL AND ANGLE SHAPES RECTANGULAR AND ROUND HSS ASTM A 500, GRADE B ASTM A 53, GRADE B **PLATES** 

ASTM A 572, GRADE 50, ASTM A 36 WHERE INDICATED

ASTM A 572, GRADE 50, ASTM A 36 WHERE INDICATED BASE PLATES ANCHOR RODS ASTM F 1554 GRADE 36, U.O.N. ASTM A 307 MACHINE BOLTS HIGH STRENGTH BOLTS ASTM A 325-N TYP. U.O.N., SC OR X WHERE INDICATED

ASTM A 108

2. STRUCTURAL STEEL SHALL CONFORM TO AISC SPECIFICATIONS FOR STRUCTURAL STEEL BUILDINGS.

3. CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR REVIEW PRIOR TO FABRICATION. FABRICATE FROM APPROVED DRAWINGS ONLY.

4. HIGH-STRENGTH BOLTS IN THE SLRS AND IN AESS SHALL BE FULLY TENSIONED. OTHER HIGH STRENGTH BOLTS SHALL BE SNUG TIGHT ONLY UNLESS OTHERWISE NOTED ON THE DRAWINGS. TENSIONED BOLT CONNECTIONS SHALL BE TENSIONED IN ACCORDANCE WITH THE SPECIFICATIONS.

5. WELDING SHALL ONLY BE PERFORMED BY CERTIFIED WELDERS. WELDING SHALL CONFORM TO AWS SPECIFICATIONS. PROVIDE TEMPORARY BACK-UP PLATES OR WELDS AT ALL COMPLETE JOINT PENETRATION (CJP) WELD LOCATIONS AS REQUIRED; REMOVE PLATES AFTER CJP WELDING AND GRIND AREA SMOOTH WHERE EXPOSED.

6. WHERE FIELD WELDING IS SPECIFICALLY NOTED, THE DESIGNATION IS GIVEN AS A SUGGESTED CONSTRUCTION PROCEDURE ONLY. CONTRACTOR SHALL DETERMINE SUITABILITY OF SHOP OR FIELD WELDING FOR ALL CONDITIONS.

7. DO NOT CUT THROUGH ERECTED STEEL PLATES, BOLTS, ANGLES OR SHAPES WITHOUT PERMISSION OF THE ARCHITECT. WHERE STEEL WILL BE EXPOSED TO VIEW, SLAG AND ROUGH EDGES SHALL BE MECHANICALLY REMOVED TO PROVIDE A SMOOTH EDGE AFTER CUTTING OR BORING. ALL SURFACES CUT BY MANUAL THERMAL PROCESSES SHALL BE GROUND (1/32 INCH MIN.) TO BRIGHT METAL.

SHOP AND FIELD WELDING SHALL BE INSPECTED BY THE UNIVERSITY'S TESTING AGENCY.

9. SPECIAL WELD PROCEDURES WILL BE REQUIRED WHERE WELDING TO EXISTING STRUCTURAL STEEL IS REQUIRED. THE WELD PROCEDURES SHALL BE PROPOSED BY THE CONTRACTOR AND SUBMITTED FOR REVIEW BY THE ARCHITECT. PROCEDURES FOR WELDING TO EXISTING STRUCTURAL STEEL SHALL BE PRE-QUALIFIED BY THE UNIVERSITY'S TESTING AGENCY IN ACCORDANCE WITH AWS D1.1.

10. WHERE STRUCTURAL STEEL IS TO BE ATTACHED USING POST-INSTALLED ANCHORS, ANCHOR HOLES SHALL BE DRILLED PRIOR TO PREPARATION OF STEEL SHOP DRAWINGS AND FABRICATION DRILLED HOLE LOCATIONS SHALL BE RECORDED AND TRANSFERRED USING TEMPLATES FOR THE PURPOSE OF ACCURATELY LOCATING HOLES IN STRUCTURAL STEEL.

11. SEE ARCHITECTURAL DRAWINGS FOR FINISHES AND SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS FOR ARCHITECTURALLY EXPOSED STRUCTURAL STEEL (AESS).

12. CUTTING AND BORING OF EXISTING STEEL SHALL NOT BE DONE EXCEPT WHERE SPECIFICALLY CALLED FOR ON THE DRAWINGS. HOLES THROUGH EXISTING STEEL MAY BE DRILLED, FLAME CUT, OR MADE USING AIR-ARC, AND SHALL NOT BE MORE THAN ½ INCH DIAMETER LARGER THAN REQUIRED TO PASS REINFORCEMENT, ANCHORS, ETC., SHOWN ON DRAWINGS, UNLESS OTHERWISE NOTED.

13. MANUAL FLAME CUTTING AND AIR-ARC CUTTING SHALL BE DONE ONLY BY CERTIFIED WELDERS. AFTER CUTTING OR BORING, SLAG AND ROUGH EDGES SHALL BE MECHANICALLY REMOVED TO PROVIDE A SMOOTH EDGE.

14. DEMAND CRITICAL WELDS: COMPLETE JOINT PENETRATION AND FULL DEPTH PARTIAL

PENETRAION WELDS AT LEVEL 9 AND BELOW SHALL BE CONSIDERED AS DEMAND CRITICAL WELDS

15.PROTECTED ZONES: THE FIRST TWO-FEET OF EACH END OF HSS BRACES AND BRACE GUSSET AND BASE PLATES SHALL BE CONSIDERED AS PROTECTED ZONES.

## **METAL DECK**

- SEE PLANS FOR DECK PROFILES.
- 2. STEEL DECK SHALL BE WELDED TO ALL STRUCTURAL STEEL AND TO ADJACENT DECK SECTIONS IN ACCORDANCE WITH THE DECK WELDING SCHEDULE. MINIMUM DECK WELDS TO STRUCTURAL STEEL SHALL BE 3/4-INCH DIAMETER FUSION WELDS AT 24 INCHES O.C. OR ALTERNATE CELLS.
- 3. WELDING OF DECK SHALL BE IN ACCORDANCE WITH AWS STANDARDS AND PERFORMED BY WELDERS CERTIFIED FOR LIGHT-GAGE METALS.
- 4. PROVIDE VENTED DECK FOR DECKS TO RECEIVE CONCRETE FILL UNLESS OTHERWISE NOTED. DECKS WITHOUT CONCRETE FILL SHALL NOT BE VENTED.

## CONCRETE

1. CONCRETE SHALL DEVELOP THE FOLLOWING COMPRESSIVE STRENGTHS AT 28 DAYS (AND 56 DAYS WHERE APPLICABLE):

56 DAYS 3000 PSI 4000 PSI DRILLED PILES 4000 PSI 5000 PSI PILE CAPS & PEDESTALS FOOTINGS, GRADE BEAMS 4000 PSI WALLS, PILASTERS 4000 PSI 4000 PSI BRIDGE PIER & CAP 4000 PSI SLABS-ON-GRADE, CURBS 4000 PSI FILL ON METAL DECK

LIGHTWEIGHT CONCRETE

FILL ON METAL DECK 4000 PSI

- 2. REFER TO SPECIFICATIONS FOR CONCRETE CLASS DESIGNATIONS.
- 3. EXPOSED CORNERS OR EDGES OF COLUMNS, PILES, WALLS, BEAMS, ETC., SHALL BE FORMED WITH A 3/4" CHAMFER UNLESS OTHERWISE NOTED ON DRAWINGS.
- CONSTRUCTION JOINTS SHALL BE LOCATED WHERE SHOWN AND, IF NOT SHOWN, WHERE DIRECTED BY THE ARCHITECT. THEY SHALL BE LOCATED SO AS TO LEAST IMPAIR THE STRENGTH OF THE STRUCTURE AND TO MINIMIZE SHRINKAGE. PROVIDE DOWELS AND KEYS AS DETAILED AND DIRECTED, AND THOROUGHLY CLEAN AND REMOVE LAITANCE FROM SURFACES BEFORE PROCEEDING WITH THE NEXT PLACEMENT.

5. CONTRACTOR SHALL SUBMIT CONSTRUCTION JOINT LAYOUT FOR REVIEW.

FOR DRIP EDGES, REGLETS, REVEALS, AND OTHER FEATURES NOT SHOWN ON THE STRUCTURAL DRAWINGS, SEE ARCHITECTURAL DRAWINGS.

## WELDED HEADED STUDS

- STEEL BEAMS SUPPORTING CONCRETE SLABS OR CONCRETE FILL ON METAL DECK SHALL HAVE WELDED STUDS IN ACCORDANCE WITH THE SCHEDULE ON THE DRAWINGS. MINIMUM SIZE AND SPACING SHALL BE 3/4" DIAMETER AT 12" O.C. UNLESS OTHERWISE NOTED.
- EACH WELDED STUD MAY REPLACE ONE DECK WELD.

## SEISMIC ISOLATORS

- SEISMIC ISOLATORS SHALL BE FRICTION PENDULUM TYPE AS MANUFACTURERD BY EARTHQUAKE PROTECTION SYSTEMS OF VALLEJO, CALFIORNIA OR APPROVED EQUAL.
- SEISMIC ISOLATORS SHALL BE DESIGNED BY A STRUCTURAL ENGINEER REGISTERED IN THE STATE OF CALIFORNIA, HIRED AND PAID BY THE CONTRACTOR, TO ACHIEVE THE TABULATED DESIGN PARAMETERS SHOWN IN THE SPECIFICATIONS.
- SEE PLANS AND SPECIFICATIONS FOR DESIGN AND DETAILING INFORMATION.
- ISOLATOR PROPERTIES: EFFECTIVE RADIUS: 167" FRICTION: 7.5% MCE DISPL.: 26"

### TENSION RESTRAINTS

- TENSION RESTRAINT DEVICES SHALL COMPLY WITH THE REQUIREMENTS OF THE DRAWINGS.
- TENSION RESTRAINT UPLIFT CAPACITY: 200-KIPS

### CONCRETE REINFORCEMENT

- . CONCRETE SHALL BE REINFORCED. REINFORCEMENT SHALL BE NEW DEFORMED STEEL BARS, ASTM A615, GRADE 60. USE ASTM A706 FOR BARS TO BE WELDED.
- CONCRETE REINFORCEMENT DETAILS SHALL CONFORM TO ACI 315, "DETAILS AND DETAILING OF CONCRETE STRUCTURES."
- 3. CONCRETE COVER SHALL BE TO FACE OF BAR, MECHANICAL COUPLER, OR WELDED HEADED BAR AS FOLLOWS, UNLESS OTHERWISE NOTED ON DRAWINGS:

CAST-IN-PLACE CONCRETE_ CAST AGAINST AND EXPOSED TO EARTH	MINIMUM CONCRETE COVER 3"
EXPOSED TO EARTH OR WEATHER #5 AND SMALLER #6 AND LARGER	1 ½" 2"
NOT EXPOSED TO WEATHER OR IN CONTACT WITH EARTH SLABS WALLS COLUMNS, BEAMS SLABS ON GRADE	1" 1 ½" 1 ½" MID-DEPTH

- CONTRACTOR SHALL SUBMIT SHOP DRAWINGS OF REINFORCEMENT LAYOUTS AND DETAILS FOR REVIEW PRIOR TO FABRICATION. SHOW ALL PROPOSED SPLICE LOCATIONS. FABRICATE FROM APPROVED DRAWINGS ONLY.
- . THE LENGTHS AND SPLICES OF REINFORCEMENT SHOWN ON DRAWINGS REPRESENT A SUGGESTED CONSTRUCTION JOINT LAYOUT. BAR SPLICES MAY BE DELETED AND CONTINUOUS REINFORCEMENT USED AT THE CONTRACTOR'S OPTION. LONG BARS OR BENT BARS SHOWN MAY BE SPLICED IF NECESSARY FOR PLACEMENT OR EASE OF CONSTRUCTION PROVIDED MINIMUM SCHEDULED LAP LENGTHS ARE FOLLOWED WITH APPROVAL FROM THE ARCHITECT. MECHANICAL COUPLERS SHALL BE USED WHERE SHOWN ON THE DRAWINGS AND MAY BE USED IN LIEU OF LAP SPLICES WITH APPROVAL FROM THE ARCHITECT.
- PROVIDE DOWELS OR CONTINUOUS REINFORCEMENT BETWEEN ALL CONCRETE ELEMENTS, UNLESS OTHERWISE NOTED. IN GENERAL, BAR SPLICES SHALL BE MADE AT POINTS OF MINIMUM STRESS. IN FRAMED BEAMS AND SLABS, SPLICE TOP BARS AT MID-SPAN, BOTTOM BARS OVER SUPPORTS, UNLESS OTHERWISE NOTED. IN GRADE BEAMS SUPPORTED ON SOIL. SPLICE TOP BARS AT COLUMNS, BOTTOM BARS AT MID-SPAN BETWEEN COLUMNS, UNLESS OTHERWISE NOTED ON DRAWINGS. IN GRADE BEAMS SUPPORTED ON PIERS OR PILES, SPLICE TOP BARS AT MID-SPAN BETWEEN SUPPORTS, BOTTOM BARS AT SUPPORTS, UNLESS OTHERWISE NOTED ON DRAWINGS. VERTICAL REINFORCEMENT FROM COLUMNS, PILASTERS AND WALLS SHALL BE DOWELED TO SUPPORTING FOOTINGS WITH BARS OF SAME SIZE AND SPACING AS VERTICAL REINFORCEMENT UNLESS OTHERWISE NOTED ON DRAWINGS.
- SPLICES OF #9 AND LARGER REINFORCEMENT SHALL BE MADE USING TYPE II MECHANICAL COUPLERS, UNLESS OTHERWISE SHOWN. LAP SPLICES FOR #9 AND LARGER BARS SHALL NOT BE
- . MECHANICAL COUPLERS SHALL NOT REQUIRE SPECIAL STIRRUPS OR HOOPS, OR VIOLATE THE REQUIRED CLEAR COVER OF CONCRETE. MECHANICAL COUPLERS SHALL BE STAGGERED A MINIMUM OF 3'-0" FROM MECHANICAL COUPLERS ON ADJACENT BARS, UNLESS OTHERWISE NOTED ON DRAWINGS.
- CONTRACTOR SHALL ORDER ADEQUATE ADDITIONAL UNITS OF REINFORCEMENT SPLICED WITH MECHANICAL COUPLERS AND ADEQUATE ADDITIONAL UNITS OF REINFORCEMENT TERMINATED WITH WELDED HEADED BARS TO FACILITATE THE MINIMUM TESTING REQUIREMENTS TO BE PERFORMED. BY THE UNIVERSITY'S TESTING AGENCY.
- 10. THE UNIVERSITY'S TESTING AGENCY SHALL TENSION TEST ONE TYPE II MECHANICAL COUPLER FOR EACH ONE HUNDRED DEVICES UTILIZED ON PROJECT. ROUND UP TO NEXT HIGHEST 100 FOR INTERMEDIATE NUMBER OF DEVICES, AND TEST A MINIMUM OF TWO DEVICES. UNIVERSITY'S TESTING AGENCY SHALL TENSION TEST ONE WELDED HEADED BAR FOR EACH ONE HUNDRED DEVICES UTILIZED ON PROJECT. ROUND UP TO NEXT HIGHEST 100 FOR INTERMEDIATE NUMBERS AND TEST TWO DEVICES MINIMUM. FAILURE OF A DEVICE SHALL REQUIRE ADDITIONAL TESTS OF ONE IN TEN DEVICES OF THE SAME HEAT OF DEVICE. ADDITIONAL REINFORCEMENT REQUIRED DUE TO FAILED DEVICES SHALL BE AT THE EXPENSE OF THE CONTRACTOR.
- 1. THE UNIVERSITY'S TESTING AGENCY SHALL TORQUE TEST TEN PERCENT OF IN-PLACE TYPE II MECHANICAL COUPLERS TO THE MANUFACTURER'S RECOMMENDED INSTALLATION TORQUE. IF ANY ONE TORQUE TEST FAILS, ALL TYPE II MECHANICAL COUPLERS INSTALLED THAT DAY SHALL BE TORQUE TESTED BY THE UNIVERSITY'S TESTING AGENCY. THE CONTRACTOR SHALL CORRECT ALL TYPE II MECHANICAL COUPLERS IDENTIFIED AS HAVING FAILED TORQUE TESTS. UNIVERSITY'S TESTING AGENCY SHALL RETEST ALL FAILED COUPLERS.
- 2. REINFORCEMENT INTERRUPTED BY STRUCTURAL STEEL SHAPES OR PLATES SHALL BE WELDED TO THE INTERRUPTING ELEMENT WITH COMPLETE JOINT PENETRATION WELDS. UNLESS OTHERWISE APPROVED BY THE ARCHITECT.

## LIST OF DRAWINGS

- S0.0.1 GENERAL NOTES S0.0.2 GENERAL NOTES
- S2.1 FOUNDATION AND LEVEL 9 PLANS S2.1.1 FOUNDATION AND LEVEL 8A & 8B S2.1.2 FOUNDATION AND LEVEL 8C & 8D

S2.1.3 FRAMING PLAN LEVEL 9A & 9B

- S2.1.4 FRAMING PLAN LEVEL 9C & 9D S2.2 LEVEL 10 & ROOF PLANS S2.2.1 FRAMING PLAN LEVEL 10A & 10B S2.2.2 FRAMING PLAN LEVEL 10C & 10D
- S2.2.3 ROOF PLANS A THRU E S2.3.1 PARTIAL PLANS S3.1.1 TRANSVERSE BUILDING SECTIONS S3.1.2 TRANSVERSE BUILDING SECTIONS
- S3.2.1 LONGITUDINAL BUILDING SECTION S3.2.2 LONGITUDINAL BUILDING SECTION S3.2.3 LONGITUDINAL BUILDING SECTION S3.2.4 LONGITUDINAL BUILDING SECTION S3.2.5 TYPICAL BRACE ELEVATIONS
- S3.3.2 3D VIEW WITH SITE S3.3.3 3D VIEW WITH SITE BUILDINGS S3.3.4 3D VIEW WITH BRIDGE S5.0.1 TYPICAL CONCRETE DETAILS
- S5.0.2 TYPICAL CONCRETE DETAILS S5.0.3 FOUNDATION DETAILS S7.0.1 TYPICAL STEEL DETAILS S7.0.2 TYPICAL STEEL DETAILS

\$3.3.1 3D VIEW AREA A & B

- S7.0.3 TYPICAL METAL DECK DETAILS S7.0.4 TYPICAL METAL DECK DETAILS S7.0.5 ISOLATOR CONNECTION DETAILS S7.0.5A ISOLATOR CONNECTION DETAILS
- S7.0.8 STEEL DETAILS S7.2.0 UPLIFT RESTRAINT DETAILS

S7.0.5B STEEL DETAILS

S7.0.6 STEEL DETAILS

S7.0.7 STEEL DETAILS

# **LEGEND**

EXISTING CONCRETE

GRADE BEAM TYPE

- ISOLATOR TYPE

 $|505'-6''| = 6'-0'' \longrightarrow MIN.$  PILE EMBED LENGTH INTO IGM

- PEDESTAL TYPE

- PILE CAP TYPE

|462'-6"|455'-2"|E=6'-0" MIN. PILE EMBED LENGTH INTO IGM

- DRILLED PILE TYPE

DP-42 | 420' ESTIMATED T.O. IGM ELEV. PER GEOTECH REPORT

T.O. PILE CAP ELEVATION

PED-A PC-4B 400' ← ESTIMATED T.O. IGM ELEV. PER GEOTECH REPORT

— T.O. PILE CAP ELEVATION

MECHANICAL COUPLER

T-HEAD REINFORCING

EDGE OF DEPRESSED

COLUMN CONNECTION

MOMENT CONNECTION

DOUBLE ROW BOLTING CONNECTION

BRIDGE TIE-BACK CONNECTION, SEE 9/S7.3.1

- HEADED STUD LAYOUT

(C=1 ½") POSITIVE OR UPWARD CAMBER AT MID-SPAN

FULL-DEPTH STIFFENER

STEEL COLUMN TYPE

BEARS ON THIS LEVEL

STEEL COLUMN BELOW.

CONNECTED TO BEAM

ON THIS LEVEL

DIAGONAL BRACING

DIAGONAL BRACING

DIAMETER IN INCHES

INDICATES ROUND WEB PENETRATION

INDICATES RECTANGULAR WEB

PENETRATION, WIDTH x HEIGHT

- METAL DECK SPAN DIRECTION

METAL DECK AND FILL TYPE

- METAL DECK SPAN DIRECTION

ELEMENT BELOW

ELEMENT ABOVE

TOP OF CONCRETE DIMENSION MEASURED

TIE-BACK CONNECTION, SEE S7.09

W16x26 1 [-8"] FROM TYPICAL TOP OF CONCRETE

C1 - STEEL COLUMN TYPE

SLAB. S.A.D. FOR DIMENSIONS

- T.O. PEDESTAL ELEVATION

CONCRETE BEAM MARK. SEE SCHEDULE

ONE-WAY SLAB MARK, SEE SCHEDULE

SIMPLE BEAM TO BEAM AND BEAM TO

NON-SEISMIC MOMENT CONNECTION

SPECIAL, SEISMIC RESISTING (SR)

BEAM TYPE

L—SLAB TYPE

- ISOLATOR DEAD LOAD (KIPS)

⊢--GB-1

**-----**

–( FP−1 | 800k <del>-}</del>

\_\_\_\_\_

ANCHOR BOLT TOP OF FOOTING, GRADE BEAM, OR MAT SLAB ABV. ABOVE ELEVATION WITH RESPECT TO TOP OF SLAB ALT. ALTERNATE ELEVATION A.R. ANCHOR ROD BLW. BELOW INDICATES SLOPE, ARROWHEAD BM. BEAM POINTS TO LOWER ELEVATION. B.N. **BOUNDARY NAILING** DESIGNATES FOOTING TYPE B.O. **BOTTOM OF** BOTT. BOTTOM **BUCKLING-RESISTING** TOP OF SLAB, WALL, ETC. ELEVATION BRACED FRAME BRG. BEARING B.S. BACK SIDE BTW/

C.I.P.

CJP

C.L.

CLR.

C.M.U.

COL.

CONC.

COND.

CONN.

CONT.

CTR'D.

C.S.

D.B.A.

DET.

DIAG.

DN.

DWG.

DWL.

E.J.

E.N.

E.P.S.

EQ.

E.S.

E.W.

EXA

FDN.

FIN.

FLG.

FLR.

F.O.C.

F.O.S.

F.O.W.

FRMG.

FTG.

GALV.

G.B.

GR.

HDR.

H.S.

HSB

LLH

LLV

MAX.

MB

N.I.C.

N.S.

N.T.S.

O.C.

O.F.

O.H.

O.S.B.

O.W.S.J.

PLY. or P.W

REINF.

REQ.

R.O.

RWD.

S.A.D.

S.C.D.

SECT.

S.E.D.

SHT

SIM.

S.J.

S.M.D.

S.M.S.

S.P.D.

SPECS.

S.R.

STD.

STIFF.

STL.

T&B

T&G

T.B.

T.F.F.

T.O.C.

T.O.S.

TYP.

U.A.

U.O.N.

V.I.F.

W/O

W.P.

W.S.

W.T.S.

W.W.F.

(V) or VERT.

SYMM.

STAGG'D.

PDF

OP'G OR OPG.

H. or HORIZ.

EL. or ELE\

DIA. OR Ø

BETWEEN CAST-IN-PLACE **CONSTRUCTION JOINT COMPLETE PENETRATION** CENTERLINE CONCRETE MASONRY UNIT COLUMN

CONCRETE

CONDITION

CONNECTION

CONTINUOUS

CENTERED

DOUBLE

DOUGLAS FIR

DIAMETER

DIAGONAL

DRAWING(S)

EACH FACE

**ELEVATION** 

END NAILING

EACH SIDE

EACH WAY

FINISH

**FLANGE** 

FLOOR

FOUNDATION

FIELD NAILING

FACE OF STUD

FACE OF WALL

FRAMING

FAR SIDE

FOOTING

**GLU-LAM** 

HORIZONTAL

HEADED STUD

INSIDE FACE

JOIST

JOINT

INTERMEDIATE GEOMATERIAL

HIGH STRENGTH BOLT

HOLLOW STRUCTURAL

LONG LEG HORIZONTAL

LONG LEG VERTICAL

LAG SCREW

MACHINE BOLT

NOT APPLICABLE

NOT IN CONTRACT

NEAR SIDE

ON CENTER

OPENING

NOT TO SCALE

OUTSIDE FACE

OPPOSITE HAND

POWDER DRIVEN

FASTENER

PLATE

PLYWOOD

PARTIAL JOINT

PENETRATION

RESIN DOWEL

REQUIRED

REDWOOD

DRAWINGS

SECTION

DRAWINGS

SEISMIC JOINT

SEE MECHANICAL

SPECIFICATIONS

SEISMIC RESISTING

SQUARE

STAGGERED

STANDARD

STIFFENER

SYMMETRICAL

TIE BEAM

TYPICAL

NOTED

VERTICAL

WITHOUT

**WORK POINT** 

WOOD SCREW

WELDED THREADED STUD

WELDED WIRE FABRIC

WITH

TOP AND BOTTOM

TONGUE AND GROOVE

TOP OF FINISHED FLOOR

TOP OF CONCRETE

UNDERCUT ANCHOR

UNLESS OTHERWISE

VERIFY IN FIELD

TOP OF STEEL

STEEL

SHEET METAL SCREW

SEE PLUMBING DRAWINGS

SHEET(S)

SIMILAR

REINFORCEMENT

ROUGH OPENING

SOLID BLOCKING

SEE ELECTRICAL

SEE ARCHITECTURAL

SEE CIVIL DRAWINGS

POST-TENSION OR

PRESSURE TREATED

OPEN WEB STEEL JOIST

MAXIMUM

MINIMUM

NEW

GRADE

HEADER

GALVANIZED

**GRADE BEAM** 

FACE OF CONCRETE

**EQUAL** 

**ECCENTRIC BRACED** 

**EXPANSION JOINT** 

**EXPANDED POLYSTYRENE** 

**EXPANSION ANCHOR** 

DOWN

DOWEL

EACH

**EXISTING** 

DETAIL

CONCRETE SCREW

DEFORMED BAR ANCHOR

**ABBREVIATIONS** 

F.650,474,1451 SMITHGROUP architecture engineering interiors planning PENNY (nail size, as in 10d) MINNEAPOLIS OFFICE

> www.smithgroup.com SAN FRANCISCO OFFICE 301 BATTERY STREET 7TH FLOOR SAN FRANCISCO, CA 94111 T 415.227.0100

> > T.707.429.5300

F.707.429.2086

SUITE 2420

T 612.372.4681

F 612.372.4957

CREEGAN + D'ANGELO INFRASTRUCTURE ENGINEERS CIVIL ENGINEER 2420 MARTIN RD SUITE 380 FAIRFIELD, CA 94534

INSTITUTE FOR REGENERATION MEDICINE BUILDING

UCSF PROJECT NUMBER:

UCSF FILE NUMBER:

DPR

DPR CONSTRUCTION, INC.

GENERAL CONTRACTOR

1450 VETERANS BOULEVARD

REDWOOD CITY, CA 94063

**60 SOUTH SIXTH STREET** 

MINNEAPOLIS, MN 55402

T.650.474.1450

FORELL/ELSESSER ENGINEERS. INC. STRUCTURAL ENGINEER 160 PINE STREET SUITE 600 SAN FRANCISCO, CA 94111 T.415.837.0700 F.415.837.0800

ACCO ENGINEERED SYSTEMS, INC.

REV DATE

<u>A</u> <u>02-27-2009</u>

F.510,347,1317 CUPERTINO ELECTRIC INC. **ELECTRICAL ENGINEER** 1740 CESAR CHAVEZ SAN FRANCISCO, CA 94124 T.415.970.3400 F.415.970.3434

ISSUED FOR

PKG. #4 - Addendum #1

<u>PKG. #6 - Permit Set</u> <u>B</u> <u>06-17-2009</u>

MECHANICAL ENGINEER

SAN LEANDRO, CA 94577

1133 ALADDIN AVENUE

T.510.346.4300

Record Drawings 09-30-2010 SEALS AND SIGNATURES ORIENTED STRAND BOARD

PROJECT NORTH

DRAWING TITLE **GENERAL** 

AS NOTED

PROJECT NUMBER

DRAWING NUMBER